

Active Vibration Isolation by Open and In-filled Trenches: A Comparative Study

Ankurjyoti Saikia

Dept. of Civil Engineering, Tezpur University

Tezpur, Assam. INDIA. asaikia@tezu.ernet.in

Abstract:Active isolation of steady-state surface vibrations by open and softer in-filled trenches in an elastic and homogeneous half-space is investigated in this study using PLAXIS 2D. Percentage isolation by barrier is estimated from amplitude reduction factors. Effects of in-fill material parameters are investigated in terms of impedance ratios against the case of a trench of definite geometry. Several cases of softer backfilled trenches with impedance ratios ranging from 0.08-0.42 are studied and their effectiveness is compared with that of an open trench of identical dimension. It is found that softer in-filled trench barriers of impedance ratios lying between 0.08-0.17 exhibit isolation effectiveness comparable to open trenches. Isolation efficiency of in-filled trenches increases with decrease in impedance ratio. Both open and in-filled trenches are found more effective in reducing the vertical vibration component than the horizontal.

Keywords:vibration isolation, in-filled trench, impedance ratio, Rayleigh wavelength

1. Introduction

Man-made ground vibrations can be mitigated by constructing barriers on the surface in the form of open/in-filled trenches, sheet piles etc. Over the past few decades, barrier isolation has extensively been investigated by several authors. Wood's experimental study on open trench [1], numerical studies of Beskos et al. [2], Leung et al. [3], and Dasgupta et al. [4] on open and in-filled trench isolation are some extensive parametric studies. Open and in-filled trench isolation [5], performance of solid wave obstacles [6], active isolation by open and in-filled trenches [7, 8] are some subsequent investigations.

Impulse load isolation by open and in-filled trenches [9], shock-induced vibration isolation by soft and stiff barriers [10] are few more studies. Vibration screening by trenches and elastic footings [11], studies of Ju [12], Di Mino et al. [13], Hung et al. [14] etc. are some investigations on train-induced vibration isolation. Experimentation on open and geofoam-filled trenches [15], isolation using water-filled trenches [16], analysis and design of open trenches [17] are contemporary studies in the arena.

Previous works primarily studied the effect of geometric parameters of concrete-filled trenches. This work, in contrast, investigates the effects of in-fill material properties on isolation response of an in-filled trench of definite geometry. Active isolation scheme is considered in this study where the barrier is placed close to the source. Several cases of softer backfill are studied and their screening performance is compared with that of and open trench and crucial conclusions are made.

2. METHODOLOGY

The half-space and backfill parameters and key steps of finite element (FE) modeling scheme are summarized in TABLE 1. Half-space and dynamic load parameters are assumed from published literature [11, 18, 19]. The Rayleigh wavelength (L_R) of vibration is estimated to be 3 m. For detailed finite element modelling, readers may refer to author's previous studies [18, 19].

Assumptions/method s/steps	Description
Half-space soil	Elastic modulus = 46000 kN/m^2 ,
parameters	density =1800 kg/m ³ , Poisson's
_	ratio=0.25, material damping =5%
In-fill material parameters	Elastic modulus =variable, density
	=1500 kg/m ³ , Poisson's ratio=0.25,
	material damping =5%
Dynamic load	Magnitude (P_0)=1 kN, frequency
parameters and type	(f)=31 Hz, type: steady-state
Type of FE model	2-D axisymmetric model of size 35 m
and size	× 15 m
Boundary conditions	Standard fixity
Absorbent	Specified to bottom and right-hand
boundaries	boundaries
Material model of	Linear elastic and 'drained' type
soil and its type	
Mesh elements	15-noded triangular elements
Mesh division	Done with 'very fine' elements
Material damping	Assigned in terms of Rayleigh mass
	and stiffness matrix coefficients
Dynamic time	0.5 s
interval	0.0 5.
Time-step of	0.0005 s.
integration	

Analyses are performed assuming a trench of depth (d)=3 m $(=1L_R)$, width (w)=1.5 m $(=0.5L_R)$ located at a distance (l) of 3 m $(=1L_R)$ from source. Effect of in-fill material parameters is studied in terms of impedance ratio $(IR = V_b \rho_b / V_s \rho_s)$. Where V_b , V_s are shear wave velocities in backfill and native soil and ρ_b , ρ_s are the corresponding densities. *IR* values are altered by changing backfill elastic modulus, keeping other parameters same.

Amplitude reduction is estimated in terms of amplitude reduction ratio (A_r) which is the ratio between maximum surface displacement amplitudes with and without barrier. A_r values are calculated at several nodes beyond the barrier (N=10) and averaged. The % isolation is finally estimated

TABLE 1: FINITE ELEMENT MODELLING SCHEME

from the average amplitude reduction ratio (A_m) as shown in Eqs. (1a)-(b).

$$A_{m} = \frac{1}{N} \sum A$$
 (1a)

% Isolation = $(1 - A_m) \ge 100$ (lb) The numerical model is validated by simulating an open trench (*IR*=0) of dimension $d=1L_R$, $w=0.1L_R$, and $l=5L_R$ and comparing with a previous study [5]. Present results are found to be in good agreement with documented results. Readers may refer to author's previous study [19] for model validation.

3. RESULTS AND DISCUSSION

Active isolation by a trench of specific geometry (depth=3 m, width=1.5 m, and distance from source=3 m) is investigated assigning different in-fill parameters. Several cases of softer in-filled trenches of different impedance ratios (*IR*=0.08, 0.17, 0.25, 0.42) and an open trench case (*IR*=0) have been investigated. Plots showing the variation of A_r against dimensionless distance from barrier (*X*=*x*/*L_R*) considering vertical and horizontal vibration components are presented in Figures. 1(a) and 1(b) respectively.

It is evident from Figures. 1(a)-(b) that softer barrier causes considerable reduction in vibration amplitudes. The amplitude reduction is governed by IR of in-fill material. Decrease in IR leads to higher amplitude reduction. The trend is similar for both horizontal and vertical vibration components. Amplitude reduction curves for IR=0.08 and 0.17 are comparable to that of an open trench of similar geometry.

Percentage (%) isolation for all these cases are finally estimated by estimating average amplitude reduction factors using Eqs. (1a)-(1b). Figure 2 shows % isolation in all these cases. It can be seen that isolation efficiency of an in-filled trench is governed by *IR* of in-fill material. Better isolation can be achieved by decreasing the *IR* value. Within a range of *IR*=0.08-0.17, in-filled trench provides isolation efficiency comparable to that of an open trench (*IR*=0).

It can also be concluded that such barriers can more effectively attenuate the vertical vibration component than the horizontal. Within a range of IR=0.08-0.17, a trench of depth, $d=3 \text{ m} (1L_R)$ in active scheme, can isolate nearly 65%-75% of the vertical vibration component and 55%-60% of the horizontal vibration component.







Figure 1(b): Amplitude reduction ratios vs. normalized distances from trench for horizontal component

The case IR=0 (that resembles an open trench) for a trench of stated dimension ($l=1L_R$, $w=0.5L_R$, and $l=1L_R$) is compared with a published literature [11]. With reference to Figure. 2, average amplitude reduction factors for vertical and horizontal vibration components are 0.3 and 0.38 respectively (% isolation 70% and 62%). Present results are in close agreements with published values of 0.3 and 0.36 for an open trench similar conFigureuration (except $w=0.33L_R$).



Figure 2: % Isolation vs. IR

4. CONCLUSIONS

Active isolation by an in-filled trench of specific dimension is investigated in this study assigning different in-fill material properties. Analyses are performed in PLAXIS 2D assuming a homogeneous and elastic half-space.

Results show that isolation efficiencies of such barriers are largely governed by impedance ratio (IR) of in-fill material. Isolation effectiveness increases with decrease in IR. Within a range of IR=0.08-0.17, an in-filled trench provides effectiveness comparable to an open trench of similar geometry.

Both open and softer barriers are more effective in isolating the vertical vibration component than the horizontal. Within IR=0.08-0.17, a trench of depth, $d=1L_R$ as an active barrier, can screen off nearly 65%-75% of the vertical vibration and 55%-60% of the horizontal vibration.

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Authors Profile



Mr. Ankurjyoti Saikia is an Assistant professor in the department of Civil Engineering at Tezpur University. His research area includes Geotechnical Engineering , Constitutive Modelling ,Soil Dynamics and Vibration Isolation. He did his MTech from IIT Kharagpur and BTech ,fromNITSilchar.

